Modified Level II Streambed-Scour Analysis for Structure I-70-69-5185 Crossing East Fork White Lick Creek in Hendricks County, Indiana

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Prepared in cooperation with the INDIANA DEPARTMENT OF TRANSPORTATION

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CONVERSION FACTORS AND ABBREVIATIONS

Multiply	Ву	To obtain
inch (in.)	25.4	millimeter
foot (ft)	0.3048	meter
square foot (ft²)	929.0	square centimeter
feet per second (ft/s)	0.3048	meters per second
cubic foot per second (ft ³ /s)	0.02832	cubic meter per second
mile (mi)	1.609	kilometer
square mile (mi ²)	2.590	square kilometer

ABBREVIATIONS used in this report:

D_{50}	median diameter of bed material
Q100	100-year discharge
FEMA	Federal Emergency Management Agency
HEC	Hydraulic Engineering Circular
IDNR	Indiana Department of Natural Resources
INDOT	Indiana Department of Transportation
USGS	United States Geological Survey
WSPRO	Water Surface PROfile model

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ABSTRACT

Level II scour evaluations follow a process in which hydrologic, hydraulic, and sediment-transport data are evaluated to calculate the depth of scour that may result when a given discharge is routed through a bridge opening. The results of the modified Level II analysis for structure I-70-69-5185 on Interstate 70 crossing East Fork White Lick Creek in Hendricks County, Indiana, are presented. The site is near the town of Camby and is in the southeastern part of Hendricks County. Scour depths were computed with the Water Surface PROfile model, version V050196, which incorporates the scour-calculation procedures outlined in Hydraulic Engineering Circular No. 18. Total scour depths at the piers were approximately 12.0 feet for the modeled discharge of 5,720 cubic feet per second and approximately 13.8 feet for the modeled discharge of 7,360 cubic feet per second.

INTRODUCTION

The U.S. Geological Survey (USGS), in cooperation with the Indiana Department of Transportation (INDOT), is conducting Level II scour analyses at a number of bridges throughout Indiana. This report describes the methods applied and the modeling results for bridge I-70-69-5185.

Background and Scope

Level I scour assessment is a process where a large number of bridges are studied as a group. Assessments usually are made by evaluating a combination of geomorphic, hydrologic, and bridge-characteristic data. The results help investigators determine which bridges appear to be most likely to experience streambed-scour problems and which bridges appear to be relatively immune to problems brought on by streambed scour (for example, bridges built on bedrock).

When applied correctly, Level I scour assessments provide an investigator with information to identify those bridges that appear to be relatively safe and those bridges that fall into higher risk categories.

Level II scour evaluations describe the process for an investigator to apply a model to a bridge site and calculate the potential depth of scour that may result from a given flood event. Level II analyses involve the application of basic hydrologic, hydraulic, and sediment-transport engineering concepts and may include an evaluation of flood history, channel hydraulic conditions (for example, water-surface profile analysis), and basic sediment-transport analyses such as scour calculations (Lagasse and others, 1995).

The methods and model outlined in Hydraulic Engineering Circular (HEC) No. 18 (Richardson and Davis, 1995) formulate the basis for Level II scour evaluations. Methods used in this study for Level II scour evaluations are a modification of the HEC-18 standards. These modifications were made to comply with the methodology requested by INDOT (Merril Dougherty, Indiana Department of Transportation, oral commun., 1996). Descriptions of the specific modifications are given in the "Evaluation Methods" section of this report.

This report presents the methods followed for modeling, special considerations for this study site, and the input for and the output from the Water Surface PROfile (WSPRO) model.

Site Description

The study site is located near the town of Camby and is in the southeastern part of Hendricks County. The drainage area for the site is approximately 34.5 mi² (estimated using Hoggatt, 1975, and USGS 7.5-minute topographic data). The predominant land use in the basin is agricultural and suburban; in the immediate vicinity of the bridge, the land is predominantly pasture with some forested land nearby.

Within the immediate vicinity of the bridge, East Fork White Lick Creek has a channel-bed slope of approximately 0.0008 ft/ft. The channel-bed material is silty sand, and the channel banks consist of silty clay. At the time of the Level I site visit on June 3, 1991, the banks were observed to have 0 to 30 percent woody vegetative cover; the field report noted that the banks were fairly stable with some small areas experiencing mass wasting.

The Interstate 70 crossing of East Fork White Lick Creek is a 111-ft-long, multi-lane bridge consisting of three spans supported by concrete and steel piers and riprap-covered spill-through abutments. Additional details describing conditions at the site are included in the Level I data base (Hopkins and Robinson, unpub. data, 1997). Photographs of the site, taken at the time of the Level I site visit, are archived at the USGS office in Indianapolis.

EVALUATION METHODS

The methods described in this section apply to a number of bridge sites in Indiana being evaluated for scour and outline the procedures requested by INDOT for these modified Level II scour analyses. The principal modification requested by INDOT was that the input data to the model come from or be estimated from existing data sources; no additional field data were collected. Actual methods used in the scour evaluation at this particular bridge site use the most applicable method possible, given the data available.

To determine drainage area, either published values found in Hoggatt (1975) or 7.5-minute topographic maps with Hoggatt's original drainage-area delineations were used. Where there are no published data, drainage-area segments measured from the maps produced by Hoggatt were either subtracted from downstream sites or added to upstream sites published by Hoggatt (1975).

In Indiana, flood discharges are coordinated by agreement among State and Federal agencies. At sites where flood discharges officially are coordinated among State and Federal agencies in Indiana, the coordinated 100-year discharge (Q100) was modeled. INDOT also provided an additional flood discharge for these coordinated sites in excess of the Q100 to be modeled.

If a flood discharge was not coordinated, the USGS examined Federal Emergency Management Agency (FEMA) studies for Q100 determinations. Where FEMA studies did not produce a Q100, the USGS contacted IDNR for an estimated Q100 in the vicinity of the site being studied. If IDNR did not have a Q100, data from nearby USGS streamflow-gaging stations were analyzed with nearby and similar drainage basins that have been coordinated. At sites having no coordinated discharge data, the two discharges used in the model were 1) the approximated Q100 and 2) a discharge equal to 1.7 times the approximated Q100.

Most of the cross-section and bridge-opening geometry data were taken from the bridge plans (Indiana State Highway Commission, 1965) provided by INDOT. Bridge plans are presumed to be representative of current conditions at the site. To determine the cross-section geometry, a line was drawn on the bridge plans parallel to the bridge stationing and approximately one bridge width from the bridge. For sites where the bridge plans did not extend far enough laterally for collection of all cross-section data required for WSPRO model analysis, additional data were collected from 7.5-minute topographic maps.

The roadway and embankment profile was taken from the bridge and highway plans for those sites where roadway overtopping was expected. The INDOT bridge plans and 7.5-minute topographic maps were used as a guide, based on the water-surface elevations calculated by the WSPRO model, to determine if roadway overtopping might occur.

Roughness values (*n*-values) for the main channel were estimated by viewing photographs archived from the Level I scour assessments. The *n*-values for the overbanks were assigned on the basis of the surface-cover data summarized in the Level I data base (Hopkins and Robinson, unpub. data, 1997). From those data, the following roughness values were assigned to the surface-cover categories: urban—0.050, suburban—0.035, row crop—0.045, pasture—0.035, brush—0.120, forest—0.100, and wetland (any area covered by standing water)—0.100. The *n*-values for the overbanks were adjusted if the Level I photographs provided sufficient detail to warrant an adjustment.

WSPRO version V050196 was used to model flow through the study site. Starting watersurface elevation was obtained with a slope-conveyance computation. The channel-bed slope in the immediate vicinity of the bridge was estimated from the 7.5-minute topographic map and was used as the slope of the energy grade line for this computation.

WSPRO version V050196 includes a field that allows the input of up to four scour-adjustment factors (K1 to K4). For this modeling, the default value for K4 (bed armoring) was chosen. For scour-adjustment factors K1 and K2 (pier-nose shape and angle of attack, respectively), input values were determined by evaluating the data archived in the Level I data base (Hopkins and Robinson, unpub. data, 1997). For the K3 factor (bed forms), a value of 1.1 was applied in all cases.

In some cases, piers set on the overbanks are constructed with footings that are higher in elevation than pier footings in the main channel. In these situations, if the channel position changes, the piers that were initially constructed on the overbank may become part of the main channel. Therefore, to evaluate total potential scour, the model results obtained for contraction scour and deepest local scour in the main channel were added and applied to all piers in the bridge opening. This methodology allowed for an evaluation of potential undermining of pier supports in the event that future channel movement placed overbank piers in the main channel.

Where bridge pairs have a continuous abutment or fill between the bridges that does not allow expansion of flow, the bridge pair was modeled as one bridge. Sites with discontinuous abutments, allowing expansion between the bridges, were modeled as two separate bridges. In those cases, a valley cross section was measured between the bridges and used as the approach section for the downstream bridge and as the exit section for the upstream bridge.

At sites with no embankment to function as a weir or at sites where the tailwater drowns out the embankment, a composite bridge and road section was used to compute flow. Those sites were computed with friction-loss equations rather than with a bridge routine.

Total scour is taken as the sum of local scour plus contraction scour. If the model predicted negative contraction scour (aggradation), the contraction-scour value was assumed to be zero in determining the total scour depth (table 1). This assumption was made so that a negative contraction scour would not mask the potentially detrimental effects of local scour at a pier. No abutment scour evaluations were made in this study.

Table 1. Cumulative scour depths for the modeled discharges at structure I-70-69-5185 crossing East Fork White Lick Creek in Hendricks County, Indiana [--, no value]

Pier number ¹	Stationing from bridge plans ²	Initial bed- elevation at pier (feet)	Main- channel contrac- tion scour depth (feet)	Local scour depth (feet)	Worst- case total- scour depth ³ (feet)	Bottom elevation of pier (feet)	Worst- case bed elevation after scour ⁴ (feet)
		Modeled o	discharge ⁵ is 5,72	0 cubic feet p	er second		-
1	295+02	702	5.9	6.1	12.0	697	688.4
2	295+45	703	5.9	6.1	12.0	697	688.4
		Modeled	discharge is 7,360	cubic feet p	er second		
1	295+02	702	7.2	6.6	13.8	697	686.6
2	295+45	703	7.2	6.6	13.8	697	686.6

¹Pier numbers were assigned from left to right as shown on the bridge plans.

SPECIAL CONSIDERATIONS

Model runs indicate the water-surface elevation at the bridge is lower than the low-steel elevation for the modeled discharges. Therefore, there should be no pressure flow through the bridge opening for the discharges modeled. Information gained by viewing the archived photographs caused the authors to slightly adjust the channel-bed material and bank stability values used for this modeling.

RESULTS

Scour depths were computed with a version of WSPRO (Larry Arneson, Federal Highway Administration, written commun., 1996) modified from Shearman (1990). This version of WSPRO includes scour calculations in the model output. Scour depths were calculated assuming an infinite depth of material that could erode and a homogeneous particle-size distribution. The results of the scour analysis are presented in table 1; a complete input file and output results are presented in the appendix.

²Stationing is the center line of the pier as determined from the bridge plans. Stationing from bridge plan, 295+02, represents a point 29,502 feet from an arbitrary starting location referenced on the bridge plans.

³Worst-case total-scour depths are generated by summing the calculated contraction-scour depth with the worst case of local scour.

⁴Worst-case bed elevation is computed by subtracting the worst-case total-scour depth from the lowest initial bed elevation in the bridge opening (700.4 feet).

⁵Not a coordinated discharge.

REFERENCES

- Hoggatt, R.E., 1975, Drainage areas of Indiana streams: U.S. Geological Survey, Water Resources Division, 231 p.
- Indiana State Highway Commission, 1965, Bridge plans Interstate Route 70: Bridge File I-70-69-5185.
- Lagasse, P.F.; Schall, J.D.; Johnson, F.; Richardson, E.V.; and Chang, F., 1995, Stream stability at highway structures (2d ed.): Federal Highway Administration, Hydraulic Engineering Circular No. 20, Publication FHWA-IP-90-014, 144 p.
- Richardson, E.V., and Davis, S.R., 1995, Evaluating scour at bridges (3d ed.): Federal Highway Administration, Hydraulic Engineering Circular No. 18, Publication FHWA-IP-90-017, 204 p.
- Shearman, J.O., 1990, User's manual for WSPRO, a computer model for water-surface profile computations: Federal Highway Administration Publication FHWA-IP-89-027, 177 p.

APPENDIX

WSPRO INPUT FILE

```
T1
          I-70 Over East Fork White Lick Creek I70-69-5185
          County: Hendricks
                                               Quad: Bridgeport 123B
Т3
          11-19-96
                                              Bret A. Robinson
SI
          0
Q
          5720 7360
          .0008 .0008
SK
XS
   EXIT 0 0
GR
          27677 720 28280 715 29348 710 29419 708 29466 708 29483 700
          29521 700 29540 708 29596 708 29647 710 29890 715 29968 720
GR
          30049 725 30551 725
GR
          .045 .100 .034 .100 .045
N
SA
          29400 29450 29540 29595
XS
   FULLV 112 0
          27677 720 28280 715 29348 710 29419 708 29466 708 29483 700
GR
          29521 700 29540 708 29596 708 29647 710 29890 715 29968 720
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          29400 29450 29540 29595
SA
    BRDGE 112 716.8 0
BR
         29470 0717.1 29470 0716.6 29473 0716.6 29508 0700.3 29543 0700.4
GR
         29577 0717.0 29580 0717.1 29581 0717.7 29581 0717.8 29576 0717.8
GR
GR
         29569 0717.6 29560 0717.2 29552 0716.5 29549 0716.2 29548 0716.2
         29544 0716.7 29538 0717.1 29530 0717.3 29522 0717.3 29513 0716.9
GR
         29506 0716.3 29504 0716.0 29502 0716.0 29497 0716.3 29491 0716.7
GR
         29483 0717.1 29476 0717.1 29472 0717.2 29470 0717.1
GR
N
         .034
         702.5 4 1
PD
         3 130 2 716.7
DC 0 BRDGE 29486 29565 29430 29680 * 4
         LPierEdge RPierEdge PierWdth * * K1 K2 K3(1.1)
         29470 29581 2 * * 1 1 1.1
DP
         29470 29581 2 * * 1 1 1.1
DP
    APPR 354 0
XS
GR
         27643 725 28695 725 28944 720 29420 715 29460 710 29493 709
         29499 708 29502 708 29512 708 29529 701 29565 701 29600 708
GR
         29667 715 29778 715 29854 720 30476 725
GR
N
         .045 .100 .034 .100 .045
         29400 29450 29620 29675
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EX
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	Federa Run Inp	l Highway Ad Model for W Date & Time: ut File: 518	ministration ater-Surface	- U.S.(Profile Cor :40 pm V Output File	Version V050196 : 5185.LST	vey
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Minimum and Maximum X, Y-coordinates
 Minimum X-Station: 27677.000 (associated Y-Elevation: 720.000)
 Maximum X-Station: 30551.000 (associated Y-Elevation: 725.000)
 Minimum Y-Elevation: 700.000 (associated X-Station: 29521.000)
 Maximum Y-Elevation: 725.000 (associated X-Station: 30049.000)
                Roughness Data ( 5 SubAreas )
                       Roughness Horizontal
               SubArea Coefficient Breakpoint
               .045
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  ********************* W S P R O ***************
     Federal Highway Administration - U. S. Geological Survey
          Model for Water-Surface Profile Computations.
          Input Units: English / Output Units: English
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       I-70 OVER EAST FORK WHITE LICK CREEK I70-69-5185
   COUNTY: HENDRICKS
                                 QUAD: BRIDGEPORT 123B
     11-19-96
                                   BRET A. ROBINSON
       *----*
             Starting To Process Header Record FULLV
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XS
    FULLV 112 0
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        27677 720 28280 715 29348 710 29419 708 29466 708 29483 700
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        29400 29450 29540 29595
    Completed Reading Data Associated With Header Record FULLV ***
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              Data Summary For Header Record FULLV
SRD Location:
                112. Cross-Section Skew: .0 Error Code
Valley Slope: .00000 Averaging Conveyance By Geometric Mean.
Energy Loss Coefficients -> Expansion: .50 Contraction: .00
                 X,Y-coordinates (14 pairs)
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  GR
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  CD
        Completed Reading Data Associated With Header Record BRDGE ***
+++072 NOTICE: X-coordinate # 2 increased to eliminate vertical segment.
+++072 NOTICE: X-coordinate # 9 increased to eliminate vertical segment.
   *** Storing Bridge Data In Temporary File As Record Number 3
                   Data Summary For Bridge Record BRDGE
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                  112. Cross-Section Skew: .0 Error Code
   SRD Location:
   Valley Slope: ******
                           Averaging Conveyance By Geometric Mean.
   Energy Loss Coefficients -> Expansion: .50 Contraction: .00
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    Minimum Y-Elevation: 700.300 (associated X-Station: 29508.000)
    Maximum Y-Elevation: 717.800 (associated X-Station: 29581.100)
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                   SubArea Coefficient Breakpoint
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1	5720.00	*****	.0008	Sub-Criti	.cal				
2	7360.00	*****	.0008	Sub-Criti	.cal				

Beginning 2 Profile Calculation(s) ******************* W S P R O ************** Federal Highway Administration - U. S. Geological Survey Model for Water-Surface Profile Computations. Input Units: English / Output Units: English *-----I-70 OVER EAST FORK WHITE LICK CREEK 170-69-5185 COUNTY: HENDRICKS QUAD: BRIDGEPORT 123B BRET A. ROBINSON 11-19-96 WSEL VHD Q AREA SRDL LEW HFV K FLEN REW EGEL НО FR # SF ALPHA ERR CRWS _____ 712.072 .324 5720.000 2106.215 ******* 28905.460 Section: EXIT 712.396 ****** 2.716 202130.00 ******* 29747.690 Header Type: XS .509 * * * * * * 2.822 707.610 ***** .000 SRD: 712.193 .298 5720.000 2210.461 112.000 28879.510 Section: FULLV Header Type: FV 712.492 .086 2.588 210620.10 112.000 29753.590 707.610 .000 SRD: 112.000 .486 .0008 2.865 .010 <<< The Preceding Data Reflect The "Unconstricted" Profile >>> .436 5720.000 1105.015 242.000 29441.130 Section: APPR 712.359 Header Type: AS 712.796 .235 5.176 159748.80 242.000 29641.720 .398 SRD: 354.000 708.435 .069 .0010 1.047 .000 <<< The Preceding Data Reflect The "Unconstricted" Profile >>> << The Following Data Reflect The "Constricted" Profile >>> <<< Beginning Bridge/Culvert Hydraulic Computations >>> WSEL VHD Q AREA SRDL LEW EGEL HFV K FLEN REW SF CRWS но FR # ALPHA ERR 711.883 1.093 5720.000 682.740 112.000 29483.130 Section: BRDGE Header Type: BR 712.976 .165 8.378 116407.90 112.000 29566.520 SRD: 112.000 708.585 .416 .517 **** 1.001 -.001 Specific Bridge Information C P/A PFELEV BLEN Bridge Type 3 Flow Type 1 -----.9993 .055 716.800 ****** ****** ****** Pier/Pile Code 0 WSEL AREA VHD Q SRDL LEW HF V K EGEL FLEN REW CRWS НО FR # SF ALPHA ERR

Section: APPR 713.190 .338 5720.000 1277.805 112.000 29434.480 713.528 .184 4.476 196821.20 121.108 29649.680 Header Type: AS SRD: 354.000 708.435 .370 .337 .0010 1.084 .015 Approach Section APPR Flow Contraction Information M(K) KQ XLKO .105 175575.8 ******* ****** 713.190 .578 <<< End of Bridge Hydraulics Computations >>> Federal Highway Administration - U. S. Geological Survey Model for Water-Surface Profile Computations. Input Units: English / Output Units: English *----* I-70 OVER EAST FORK WHITE LICK CREEK I70-69-5185 QUAD: BRIDGEPORT 123B COUNTY: HENDRICKS 11-19-96 BRET A. ROBINSON SRDL AREA WSEL VHD Q LEW HF V K FLEN REW EGEL CRWS HO FR # SF ALPHA 712.812 .323 7360.000 2801.197 ******* 28747.410 Section: EXIT 713.135 ****** 2.627 259973.90 ******* 29783.650 Header Type: XS 709.495 ***** ***** .489 SRD: .000 3.008 .297 Section: FULLV 712.930 7360.000 2925.539 112.000 28722.150 112.000 29789.400 Header Type: FV 713.227 .086 2.516 270644.40 SRD: 112.000 709.495 .000 .466 .0008 3.022 .007 <<< The Preceding Data Reflect The "Unconstricted" Profile >>> .585 7360.000 1245.594 Section: APPR 713.040 242.000 29435.680 713.625 .255 5.909 189851.00 242.000 29648.240 Header Type: AS SRD: 354.000 709.598 .144 .447 .0011 1.077 - .002 <<< The Preceding Data Reflect The "Unconstricted" Profile >>> <<< The Following Data Reflect The "Constricted" Profile >>> <<< Beginning Bridge/Culvert Hydraulic Computations >>>

	WSEL EGEL CRWS	VHD HF HO	Q V FR #	AREA K SF	SRDL FLEN ALPHA	LEW REW ERR
Section: BRDGE Header Type: BR	712.498	1.642	7360.000	734.841 128829.10		29481.810 29567.780
SRD: 112.000	709.842	.814	.620	*****	1.053	001

Specific Bridge Bridge Type 3	Information	С	P/A	PFELEV	BLEN	XLAB	XRAB
Pier/Pile Code		.9746	.054	716.800	*****	* *****	** ******
	WSEL EGEL CRWS	HF HO	FR #		SF	FLEN ALPHA	REW ERR
Section: APPR Header Type: AS SRD: 354.000	714.838	.398 .207	7360.0 4.	000 15 716 258	60.492 971.60	112.000 120.716	29661.640
М (proach Section	KQ	2	KLKQ	XRKQ	OTEL	
	.587 .169	21483	39.3 ***	*****	*****	714.440	
Federal I Mo Ing * I-70 O	Contraction S	nistrati er-Surfa nglish K WHITE	on - ace Prof / Outr LICK Cr	U. S. Gerile Compout Units REEK 170 QUAD: BRET	eological putations s: Englis 	Survey 123B SON	*
Tot	Material Tr	ansport h Value	Mode I	Factor ()	Pw): 4.0	64 00	
# Depth Conti	Flow	Contr	act App	roach S	Side Co	ntract A	Approach
1 5.934 5720 Approac 2 7.238 7360 Approac	000 5720.00 ch Channel De	00 75. pth: 00 75. pth:	000 25 5.111 000 25 6.234	0.000 I H 60.000 I	Left: ** Right: ** Left: ** Right: **	* * * * * * * * * * * * * * * * * * *	****** ****** *****
********* Federal H Mo	*************** Highway Admin odel for Wate out Units: En	* W S istrati er-Surfa	PRO on -	********* U. S. Ge	******* eological outations	****** Survey	

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I-70 OVER EAST FORK WHITE LICK CREEK 170-69-5185
   COUNTY: HENDRICKS
                                 QUAD: BRIDGEPORT 123B
      11-19-96
                                   BRET A. ROBINSON
      *** Pier Scour Calculations for Header Record BRDGE ***
                Constants and Input Variables
                    Pier Width: 2.000
          *----*
            Pier Shape Factor
                                  (K1): 1.00
            Flow Angle of Attack Factor (K2): 1.00
                                   (K3): 1.10
            Bed Condition Factor
            Bed Material Factor
                                  (K4): 1.00
           Velocity Multiplier
                                  (VM): 1.00
                                  (YM): 1.00
            Depth Multiplier
          *-----
   Scour ---- Localized Hydraulic Properties ---- -- X-Stations --
                 WSE Depth Velocity Froude #
                                            Left
   ....
   6.115720.000712.25311.9539.806.50029470.00029581.0006.637360.000712.98912.68911.646.57629470.00029581.000
   6.63
2
   ******************* W S P R O ****************
     Federal Highway Administration - U. S. Geological Survey
          Model for Water-Surface Profile Computations.
          Input Units: English / Output Units: English
   *-----
       I-70 OVER EAST FORK WHITE LICK CREEK 170-69-5185
   COUNTY: HENDRICKS
                                 OUAD: BRIDGEPORT 123B
     11-19-96
                                   BRET A. ROBINSON
      *** Pier Scour Calculations for Header Record BRDGE ***
                Constants and Input Variables
                   Pier Width: 2.000
                             (K1): 1.00
           Pier Shape Factor
           Flow Angle of Attack Factor (K2): 1.00
           Bed Condition Factor
                                  (K3): 1.10
           Bed Material Factor
                                  (K4): 1.00
                                  (VM): 1.00
           Velocity Multiplier
           Depth Multiplier
                                  (YM): 1.00
   Scour --- Localized Hydraulic Properties --- -- X-Stations --
  Depth Flow WSE Depth Velocity Froude # Left Right
  -----
  6.11 5720.000 712.253 11.953 9.806 .500 29470.000 29581.000
```

2	6.63	7360.000	712.989	12.689	11.646	.576	29470.000	29581.000
ER								
*	*****	*****	Normal e	end of V	WSPRO exec	cution.	*****	*****
*	*****	*****	lapsed Tir	ne: 0	Minutes	5 Seconds	s *****	*****